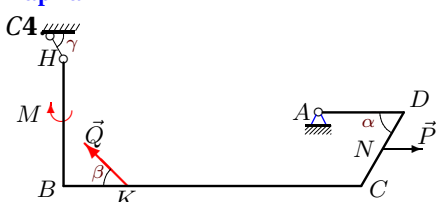
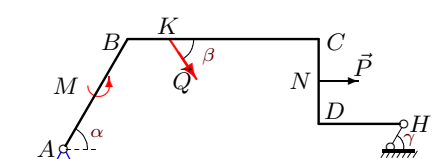
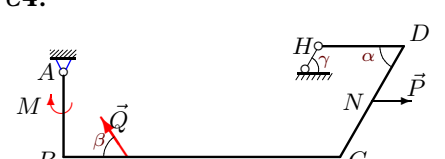
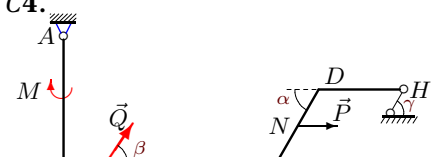
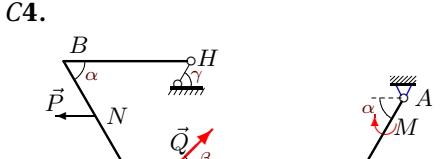
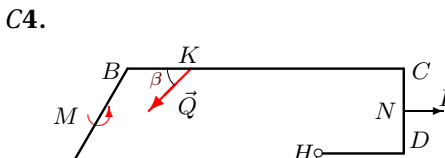


## Равновесие тяжелой рамы

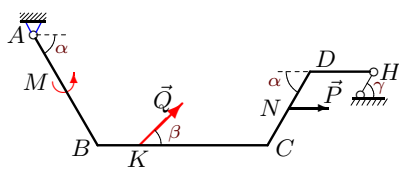
Тяжелая однородная рама расположена в вертикальной плоскости и опирается на неподвижный шарнир  $A$  и наклонный невесомый стержень  $H$ . К раме приложены горизонтальная сила  $P$ , наклонная сила  $Q$  и момент  $M$ . Учитывая погонный вес рамы  $\rho$ , найти реакции опор.

*Кирсанов М.Н. Решебник. Теоретическая механика с. 31.*

<p><b>Вариант 1</b></p> <p>C4.</p> 	<p><math>\rho = 3 \text{ кН/м}, P = 8 \text{ кН},</math>  <math>Q = 33 \text{ кН}, M = 25 \text{ кНм},</math>  <math>\alpha = 60^\circ, \beta = 45^\circ, \gamma = 60^\circ,</math>  <math>HB = 6 \text{ м}, BC = 14 \text{ м},</math>  <math>CD = 4 \text{ м}, DA = 4 \text{ м},</math>  <math>BK = 3 \text{ м}, CN = 2 \text{ м}.</math></p>
<p><b>Вариант 2</b></p> <p>C4.</p> 	<p><math>\rho = 2 \text{ кН/м}, P = 8 \text{ кН},</math>  <math>Q = 12 \text{ кН}, M = 50 \text{ кНм},</math>  <math>\alpha = 60^\circ, \beta = 60^\circ, \gamma = 45^\circ,</math>  <math>AB = 6 \text{ м}, BC = 9 \text{ м},</math>  <math>CD = 4 \text{ м}, DH = 4 \text{ м},</math>  <math>BK = 2 \text{ м}, CN = 2 \text{ м}.</math></p>
<p><b>Вариант 3</b></p> <p>C4.</p> 	<p><math>\rho = 2 \text{ кН/м}, P = 8 \text{ кН},</math>  <math>Q = 30 \text{ кН}, M = 20 \text{ кНм},</math>  <math>\alpha = 60^\circ, \beta = 60^\circ, \gamma = 45^\circ,</math>  <math>AB = 4 \text{ м}, BC = 13 \text{ м},</math>  <math>CD = 6 \text{ м}, DH = 4 \text{ м},</math>  <math>BK = 3 \text{ м}, CN = 3 \text{ м}.</math></p>
<p><b>Вариант 4</b></p> <p>C4.</p> 	<p><math>\rho = 1 \text{ кН/м}, P = 7 \text{ кН},</math>  <math>Q = 28 \text{ кН}, M = 15 \text{ кНм},</math>  <math>\alpha = 60^\circ, \beta = 60^\circ, \gamma = 30^\circ,</math>  <math>AB = 6 \text{ м}, BC = 10 \text{ м},</math>  <math>CD = 4 \text{ м}, DH = 4 \text{ м},</math>  <math>BK = 2 \text{ м}, CN = 2 \text{ м}.</math></p>
<p><b>Вариант 5</b></p> <p>C4.</p> 	<p><math>\rho = 3 \text{ кН/м}, P = 8 \text{ кН},</math>  <math>Q = 25 \text{ кН}, M = 25 \text{ кНм},</math>  <math>\alpha = 60^\circ, \beta = 45^\circ, \gamma = 60^\circ,</math>  <math>HB = 6 \text{ м}, BC = 6 \text{ м},</math>  <math>CD = 11 \text{ м}, DA = 4 \text{ м},</math>  <math>CK = 2 \text{ м}, CN = 3 \text{ м}.</math></p>
<p><b>Вариант 6</b></p> <p>C4.</p> 	<p><math>\rho = 2 \text{ кН/м}, P = 6 \text{ кН},</math>  <math>Q = 12 \text{ кН}, M = 50 \text{ кНм},</math>  <math>\alpha = 60^\circ, \beta = 30^\circ, \gamma = 45^\circ,</math>  <math>AB = 6 \text{ м}, BC = 13 \text{ м},</math>  <math>CD = 4 \text{ м}, DH = 4 \text{ м},</math>  <math>BK = 3 \text{ м}, CN = 2 \text{ м}.</math></p>

**Вариант 7**

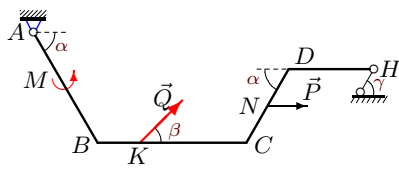
C4.



$\rho = 1 \text{ кН/м}$ ,  $P = 5 \text{ кН}$ ,  
 $Q = 19 \text{ кН}$ ,  $M = 30 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 30^\circ$ ,  $\gamma = 30^\circ$ ,  
 $AB = 6 \text{ м}$ ,  $BC = 8 \text{ м}$ ,  
 $CD = 4 \text{ м}$ ,  $DH = 3 \text{ м}$ ,  
 $BK = 2 \text{ м}$ ,  $CN = 2 \text{ м}$ .

**Вариант 8**

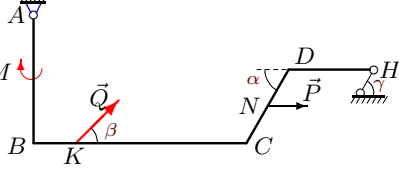
C4.



$\rho = 1 \text{ кН/м}$ ,  $P = 5 \text{ кН}$ ,  
 $Q = 20 \text{ кН}$ ,  $M = 30 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 30^\circ$ ,  $\gamma = 30^\circ$ ,  
 $AB = 6 \text{ м}$ ,  $BC = 7 \text{ м}$ ,  
 $CD = 4 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $BK = 2 \text{ м}$ ,  $CN = 2 \text{ м}$ .

**Вариант 9**

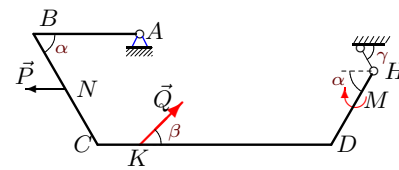
C4.



$\rho = 1 \text{ кН/м}$ ,  $P = 5 \text{ кН}$ ,  
 $Q = 30 \text{ кН}$ ,  $M = 15 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 30^\circ$ ,  $\gamma = 30^\circ$ ,  
 $AB = 6 \text{ м}$ ,  $BC = 10 \text{ м}$ ,  
 $CD = 4 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $BK = 2 \text{ м}$ ,  $CN = 2 \text{ м}$ .

**Вариант 10**

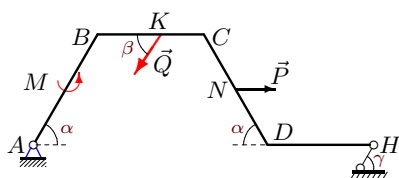
C4.



$\rho = 2 \text{ кН/м}$ ,  $P = 6 \text{ кН}$ ,  
 $Q = 25 \text{ кН}$ ,  $M = 20 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 30^\circ$ ,  $\gamma = 45^\circ$ ,  
 $AB = 5 \text{ м}$ ,  $BC = 6 \text{ м}$ ,  
 $CD = 11 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 11**

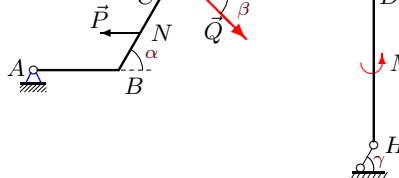
C4.



$\rho = 2 \text{ кН/м}$ ,  $P = 8 \text{ кН}$ ,  
 $Q = 20 \text{ кН}$ ,  $M = 50 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 45^\circ$ ,  
 $AB = 6 \text{ м}$ ,  $BC = 5 \text{ м}$ ,  
 $CD = 6 \text{ м}$ ,  $DH = 5 \text{ м}$ ,  
 $BK = 3 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 12**

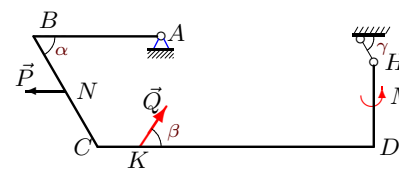
C4.



$\rho = 1 \text{ кН/м}$ ,  $P = 5 \text{ кН}$ ,  
 $Q = 14 \text{ кН}$ ,  $M = 30 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 30^\circ$ ,  $\gamma = 30^\circ$ ,  
 $AB = 4 \text{ м}$ ,  $BC = 4 \text{ м}$ ,  
 $CD = 10 \text{ м}$ ,  $DH = 7 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 2 \text{ м}$ .

**Вариант 13**

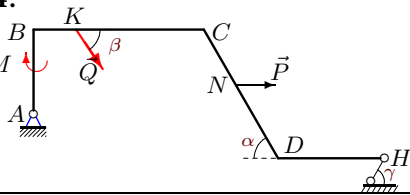
C4.



$\rho = 2 \text{ кН/м}$ ,  $P = 8 \text{ кН}$ ,  
 $Q = 13 \text{ кН}$ ,  $M = 50 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 45^\circ$ ,  
 $AB = 6 \text{ м}$ ,  $BC = 6 \text{ м}$ ,  
 $CD = 13 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 14**

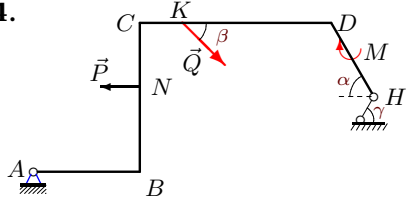
C4.



$\rho = 2 \text{ кН/м}$ ,  $P = 8 \text{ кН}$ ,  
 $Q = 29 \text{ кН}$ ,  $M = 20 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 45^\circ$ ,  
 $AB = 4 \text{ м}$ ,  $BC = 8 \text{ м}$ ,  
 $CD = 7 \text{ м}$ ,  $DH = 5 \text{ м}$ ,  
 $BK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 15**

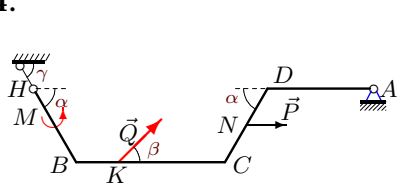
C4.



$\rho = 1 \text{ кН/м}$ ,  $P = 6 \text{ кН}$ ,  
 $Q = 35 \text{ кН}$ ,  $M = 15 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 45^\circ$ ,  $\gamma = 30^\circ$ ,  
 $AB = 5 \text{ м}$ ,  $BC = 7 \text{ м}$ ,  
 $CD = 9 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 16**

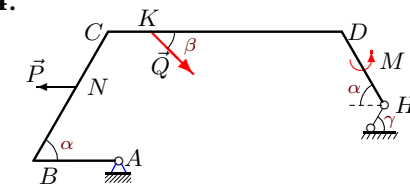
C4.



$\rho = 3 \text{ кН/м}$ ,  $P = 8 \text{ кН}$ ,  
 $Q = 16 \text{ кН}$ ,  $M = 70 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 45^\circ$ ,  $\gamma = 60^\circ$ ,  
 $HB = 4 \text{ м}$ ,  $BC = 7 \text{ м}$ ,  
 $CD = 4 \text{ м}$ ,  $DA = 5 \text{ м}$ ,  
 $BK = 2 \text{ м}$ ,  $CN = 2 \text{ м}$ .

**Вариант 17**

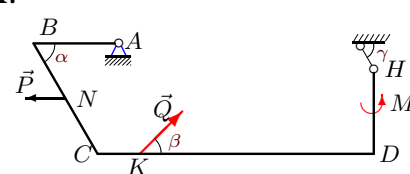
C4.



$\rho = 2 \text{ кН/м}$ ,  $P = 6 \text{ кН}$ ,  
 $Q = 16 \text{ кН}$ ,  $M = 50 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 30^\circ$ ,  $\gamma = 45^\circ$ ,  
 $AB = 4 \text{ м}$ ,  $BC = 7 \text{ м}$ ,  
 $CD = 11 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 18**

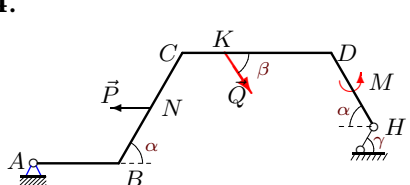
C4.



$\rho = 2 \text{ кН/м}$ ,  $P = 6 \text{ кН}$ ,  
 $Q = 14 \text{ кН}$ ,  $M = 50 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 30^\circ$ ,  $\gamma = 45^\circ$ ,  
 $AB = 4 \text{ м}$ ,  $BC = 6 \text{ м}$ ,  
 $CD = 13 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 19**

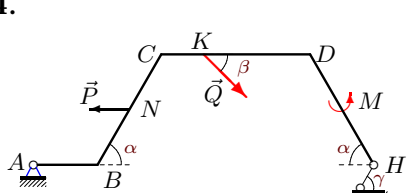
C4.



$\rho = 2 \text{ кН/м}$ ,  $P = 8 \text{ кН}$ ,  
 $Q = 19 \text{ кН}$ ,  $M = 50 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 45^\circ$ ,  
 $AB = 4 \text{ м}$ ,  $BC = 6 \text{ м}$ ,  
 $CD = 7 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 20**

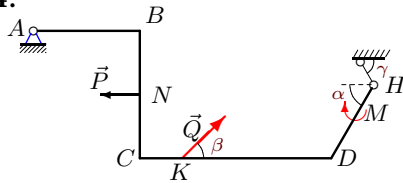
C4.



$\rho = 1 \text{ кН/м}$ ,  $P = 6 \text{ кН}$ ,  
 $Q = 19 \text{ кН}$ ,  $M = 30 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 45^\circ$ ,  $\gamma = 30^\circ$ ,  
 $AB = 3 \text{ м}$ ,  $BC = 6 \text{ м}$ ,  
 $CD = 7 \text{ м}$ ,  $DH = 6 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 21**

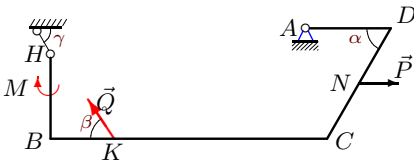
C4.



$\rho = 2 \text{ кН/м}$ ,  $P = 7 \text{ кН}$ ,  
 $Q = 28 \text{ кН}$ ,  $M = 20 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 45^\circ$ ,  $\gamma = 45^\circ$ ,  
 $AB = 5 \text{ м}$ ,  $BC = 6 \text{ м}$ ,  
 $CD = 9 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 22**

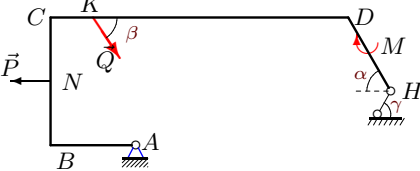
C4.



$\rho = 3 \text{ кН/м}$ ,  $P = 9 \text{ кН}$ ,  
 $Q = 34 \text{ кН}$ ,  $M = 25 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 60^\circ$ ,  
 $HB = 4 \text{ м}$ ,  $BC = 13 \text{ м}$ ,  
 $CD = 6 \text{ м}$ ,  $DA = 4 \text{ м}$ ,  
 $BK = 3 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 23**

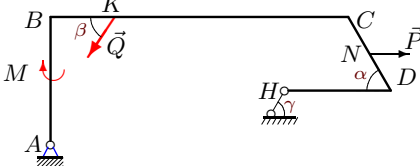
C4.



$\rho = 1 \text{ кН/м}$ ,  $P = 7 \text{ кН}$ ,  
 $Q = 31 \text{ кН}$ ,  $M = 15 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 30^\circ$ ,  
 $AB = 4 \text{ м}$ ,  $BC = 6 \text{ м}$ ,  
 $CD = 14 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 24**

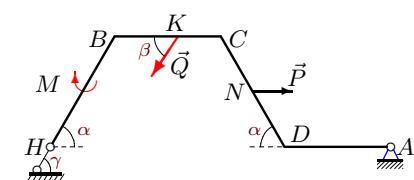
C4.



$\rho = 1 \text{ кН/м}$ ,  $P = 7 \text{ кН}$ ,  
 $Q = 27 \text{ кН}$ ,  $M = 15 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 30^\circ$ ,  
 $AB = 6 \text{ м}$ ,  $BC = 14 \text{ м}$ ,  
 $CD = 4 \text{ м}$ ,  $DH = 5 \text{ м}$ ,  
 $BK = 3 \text{ м}$ ,  $CN = 2 \text{ м}$ .

**Вариант 25**

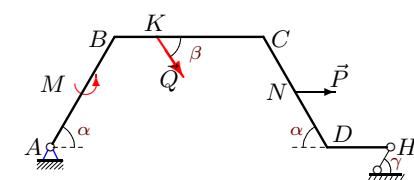
C4.



$\rho = 3 \text{ кН/м}$ ,  $P = 9 \text{ кН}$ ,  
 $Q = 23 \text{ кН}$ ,  $M = 25 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 60^\circ$ ,  
 $HB = 6 \text{ м}$ ,  $BC = 5 \text{ м}$ ,  
 $CD = 6 \text{ м}$ ,  $DA = 5 \text{ м}$ ,  
 $BK = 3 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 26**

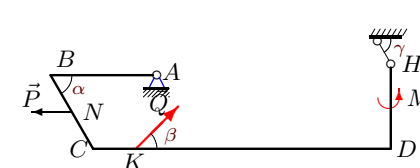
C4.



$\rho = 2 \text{ кН/м}$ ,  $P = 8 \text{ кН}$ ,  
 $Q = 21 \text{ кН}$ ,  $M = 50 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 45^\circ$ ,  
 $AB = 6 \text{ м}$ ,  $BC = 7 \text{ м}$ ,  
 $CD = 6 \text{ м}$ ,  $DH = 3 \text{ м}$ ,  
 $BK = 2 \text{ м}$ ,  $CN = 3 \text{ м}$ .

**Вариант 27**

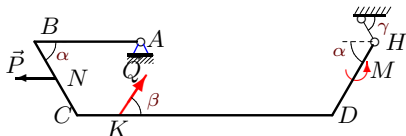
C4.



$\rho = 2 \text{ кН/м}$ ,  $P = 6 \text{ кН}$ ,  
 $Q = 13 \text{ кН}$ ,  $M = 50 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 30^\circ$ ,  $\gamma = 45^\circ$ ,  
 $AB = 5 \text{ м}$ ,  $BC = 4 \text{ м}$ ,  
 $CD = 14 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 2 \text{ м}$ .

**Вариант 28**

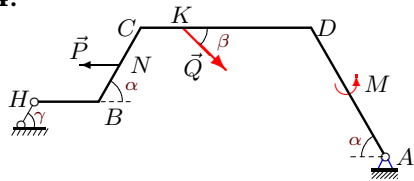
C4.



$\rho = 1 \text{ кН/м}$ ,  $P = 7 \text{ кН}$ ,  
 $Q = 18 \text{ кН}$ ,  $M = 30 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 30^\circ$ ,  
 $AB = 5 \text{ м}$ ,  $BC = 4 \text{ м}$ ,  
 $CD = 12 \text{ м}$ ,  $DH = 4 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 2 \text{ м}$ .

**Вариант 29**

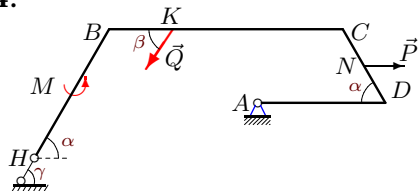
C4.



$\rho = 3 \text{ кН/м}$ ,  $P = 8 \text{ кН}$ ,  
 $Q = 20 \text{ кН}$ ,  $M = 70 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 45^\circ$ ,  $\gamma = 60^\circ$ ,  
 $HB = 3 \text{ м}$ ,  $BC = 4 \text{ м}$ ,  
 $CD = 8 \text{ м}$ ,  $DA = 7 \text{ м}$ ,  
 $CK = 2 \text{ м}$ ,  $CN = 2 \text{ м}$ .

**Вариант 30**

C4.



$\rho = 3 \text{ кН/м}$ ,  $P = 9 \text{ кН}$ ,  
 $Q = 16 \text{ кН}$ ,  $M = 70 \text{ кНм}$ ,  
 $\alpha = 60^\circ$ ,  $\beta = 60^\circ$ ,  $\gamma = 60^\circ$ ,  
 $HB = 7 \text{ м}$ ,  $BC = 11 \text{ м}$ ,  
 $CD = 4 \text{ м}$ ,  $DA = 6 \text{ м}$ ,  
 $BK = 3 \text{ м}$ ,  $CN = 2 \text{ м}$ .

Ответы

	$M_A(Q)$	$M_A(P)$	$\Sigma_k M_A(G_k)$	$h$	$X_A$	$Y_A$	$R_H$
1	-290.844	13.856	366.0	-9.124	18.842	54.590	7.016
2	-83.138	-25.569	-361.0	10.468	-42.351	28.041	40.095
3	17.942	11.215	-455.0	7.639	-34.267	-13.248	58.360
4	132.497	29.876	-150.0	10.196	-21.223	-0.378	0.258
5	-133.217	-6.928	754.5	-9.526	-40.611	9.745	61.866
6	18.000	-19.177	-505.0	7.639	-37.831	17.776	59.713
7	133.000	17.321	-156.5	9.500	-19.283	12.754	-2.507
8	140.000	17.321	-154.5	9.500	-19.329	12.727	-3.455
9	185.885	21.340	-150.0	10.196	-27.394	11.071	-4.141
10	112.500	-15.588	-90.0	6.553	-14.238	38.088	1.997
11	-51.962	-20.785	-322.0	11.314	-19.547	39.774	30.472
12	-98.000	8.660	-250.0	11.062	-31.342	18.018	27.964
13	22.517	-20.785	-81.0	6.225	4.824	43.417	4.701
14	-108.229	-11.215	-340.5	13.125	-48.356	47.259	36.566
15	-346.482	24.000	-193.0	4.938	-111.788	-3.967	107.432
16	-96.573	13.856	510.0	-13.856	-1.370	17.606	35.888
17	-96.000	20.785	-154.5	7.002	-26.006	41.850	25.667
18	70.000	-15.588	-193.0	7.639	2.075	38.800	11.596
19	-197.454	20.785	-349.0	10.089	-34.838	25.116	47.147
20	-177.291	15.588	-185.0	8.000	-41.719	15.641	39.588
21	257.387	-21.000	-376.0	9.521	-0.944	16.346	16.765
22	-353.338	23.383	289.5	-10.990	5.022	56.713	-5.956
23	-39.306	21.000	-54.0	3.804	-28.377	43.371	22.952
24	10.852	-29.876	-225.5	3.304	-61.528	13.107	78.552
25	258.942	-23.383	573.0	-13.856	-25.774	36.946	56.548
26	-145.492	-20.785	-334.0	11.314	-46.642	34.044	39.799
27	32.500	-10.392	-143.0	8.157	0.887	41.355	8.691
28	15.588	-12.124	-47.5	5.500	0.210	8.136	2.552
29	48.618	34.641	501.8	-15.588	-27.152	43.753	42.019
30	83.138	-15.588	119.2	-7.794	-17.474	69.323	32.947